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Determination of exposure to electric fields in extra high voltage substations

by K. G. LÖVSTRAND, Ph.D.¹

LÖVSTRAND, K. G. Determination of exposure to electric fields in extra high voltage substations. *Scand. j. work environ. & health* 3 (1976) 190—198. Electro-physical effects related to extra high voltage are surveyed for the determination of the exposure of personnel to electric fields in substations. It is concluded that the electric field strengths and the electrical discharges to the personnel are the important electrophysical factors. Instruments for measuring the field strength at grounded surfaces and at nonzero potentials were constructed. Results are presented of measurements with these instruments in substations. A dummy was used for the measurement of the distribution of capacitive currents to a man. The dummy can also be used for measuring the effectiveness of special shielding clothes.

Key words: extra high voltage, transmission line, substation, exposure, personnel, electric field measurement, discharge, capacitive current.

Some investigations have indicated that the exposure of personnel, working in extra high voltage (EHV)² substations, to high electric field strengths of power frequency (50 Hz or 60 Hz) may cause physiological changes (2, 7, 10). The results led to a Soviet limitation of the occupational exposure to high field strengths in EHV switchyards and near EHV transmission lines.

Several similar studies have been made, however, in which no significant physiological effects were observed (17). Some laboratory experiments on mice have shown reversible physiological effects of long-time exposure to high electric field strengths (13), whereas others have not shown any significant effects. High volt-

age constructions are surrounded by electric fields, the strength and extension of which are dependent on the operating voltage and the dimensions of the construction. Higher voltages have resulted in more pronounced effects (7, 8, 10).

The maximum voltage of main EHV transmission lines in Sweden is at present 400 kV, but a 800 kV transmission line is under construction and should be in operation within a few years.

In 1974 the Swedish State Power Board, in cooperation with the National Board of Occupational Safety and Health and the Research Institute of Electricity, started physiological, psychological, and physical investigations of the effects of electric fields on personnel in Swedish EHV substations. The investigations are expected to show if special precautions, such as shielding clothes or permanent or mobile electric shields, are necessary for the protection of the personnel working in the vicinity of the 800 kV constructions.

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² EHV = 130 kV — 800 kV.

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The present report presents the electrophysical phenomena and effects related to the EHV and the instruments which were developed for the determination of occupational exposure to electric fields in substations.

MATERIAL AND METHODS

Electrophysical effects caused by EHV

For the physical part of the investigation a survey was made of the electrophysical effects caused by EHV. The aim was to find relevant physical parameters which might be related to the medical observations made during the investigation.

With the support of previous investigations some effects could be excluded from the study.

Corona discharges occur at surfaces with a high field strength, such as wire conductors and disconnector busbars. The number of corona discharges increases during certain weather conditions, such as drizzle or misty weather.

Corona discharges produce a large number of air ions and also ozone. The physiological effects of an increased air ion density are not well known, but some investigations have shown negative health effects at high air ion concentrations (9, 11).

The increase in the air ion density was not very high a few meters away from outdoor AC EHV constructions. Air ions were thus excluded from the investigation.

An investigation by Fern and Brabets (6) showed that no significant increase in ozone concentration is to be expected near outdoor EHV constructions such as transmission lines or substations.

Electric conductors, e.g., in transmission lines with current flowing through them, are surrounded by magnetic fields. The flux density B depends on the distance r to a conductor and on the current I flowing through it. $B(r)$ can easily be calculated for a single straight conductor of infinite length.

$$B(r) = \mu_0 I / 2 \pi r, \quad (1)$$

where $\mu_0 = 4\pi \cdot 10^{-7}$ (Vs/Am).

The maximum currents in EHV transmission lines are on the order of 1,000 A, and the safety distance to EHV conductors is about 3 m. If $r = 3$ m and $I = 1,000$ A equation 1 gives $B = 6 \cdot 10^{-5}$ T.

The magnetic flux density limit (VLF) recommended for "long-time" occupational exposure is $2 \cdot 10^{-2}$ T at the Stanford Linear Accelerator Center in the U.S.A. and $3 \cdot 10^{-2}$ T in the U.S.S.R. (12). The flux density near a current-carrying conductor is thus more than two orders of magnitude below the recommended maximum exposure values. The health effect, if any, should thus be negligible during ordinary work at the constructions. Certain "hot-line" operations bring the personnel very close to the current-carrying conductors. Such operations require special attention.

The electromagnetic radio noise emission from the corona discharges was not considered to be intense enough to have any influence on the medical parameters studied (16). Exposure to high electric field strengths in work areas at EHV constructions is the factor that has been considered the most important for suspected negative health effects (13). Capacitive coupling of the AC voltage to a man standing in the electric field gives rise to a capacitive current which flows through his conducting body. This current can be 0.1—1 mA.

If an insulated person standing in the electric field touches a grounded object, he may feel a discharge at the point of contact. In such very short ($\tau < 1 \mu s$) discharges the peak current, which depends on the field strength acting on the person and the impedance of the contact (the series impedance of the discharge channel, the skin, and the body), can be about 10 A (8). Such occurrences are well known to personnel working in EHV substations. Accidents have also occurred because of the uncontrollable jerks which follow strong discharges. In a work made by Filippov and Morozov (8) the mean lower limit of the field strength for painful discharges was found to be 5.2 kV/m. The intensity of a discharge depends on the mean electric field strength acting on the person, his capacitance to earth, and the phase of the alternating electric

field at the moment of contact. The last factor will cause the discharge energy to vary in a series of contacts, even if the capacitance and the field strength are constant. The statistical distribution of the discharge energy can be calculated from the capacitance to earth and the field strength. A slow speed of touching the grounded surface can cause a series of discharges to occur for each contact, one for each half-period of the alternating electric field (8).

It was concluded from this review of the physical effects related to EHV that the electric field strength, the capacitive currents, and the electric discharges to persons were the parameters which most justified being studied.

Electric field theory

It is comparatively simple to calculate the electric field in some electrode geometries. The electric field E between a straight conductor above the ground can be obtained from three equations. The first yields the charge density q in the conduc-

tor as a function of the voltage V and the capacitance to the ground C :

$$q = V/C. \quad (2)$$

The second yields the capacitance C as a function of the height h and radius r of the conductor:

$$C = 1/2 \pi \epsilon_0 \ln (2 h/r), \quad (3)$$

and the third yields the electric field strength E as a function of q , h , and the horizontal distance x to the field strength point:

$$E = 2 qh/4 \pi \epsilon_0 (h^2 + x^2), \quad (4)$$

where $\epsilon_0 = 10^{-9}/36 \pi$. (As/Vm)

One single EHV transmission line consists however of three phase conductors and at least one ground wire. The alternating voltage of the phase conductors shifts 120° in phase angle for each "phase." Accordingly the resulting electric field at any space point is a sum of three field vectors with a 120° phase difference. The electric field vectors from the conductors are disturbed in magnitude and direction by the presence of the other conductors, the ground wire, and the ground. The field is further disturbed near the towers of the line. Calculations of the electric field strength at the ground level under transmission lines have been made by several authors (1, 15). The calculations are complicated when several conductors cross each other and several objects on the ground disturb the field.

Approximate calculations can be made of the electric field strength at the surface of conducting objects on the ground near EHV constructions. Deno (4, 5) has reported methods for several such approximations. He has also shown how the capacitive currents can be calculated with approximate geometries. The currents can be very dangerous or even fatal. Accidents have occurred when persons have touched large insulated conducting objects or insulated construction parts and have thus formed a short circuit of a sometimes fatal capacitive current to the ground.

For field and capacitive current calculations a person standing on the ground can be approximated with a semispheroid, a spheroid, or a cylinder with a hemisphere at the top end. The influence of the

Fig. 1. Capacitive current I_c to a semispheroid exposed to a 50-Hz electric field. ($E_0 = 1$ kV/m, h = the height of the spheroid in millimeters).

Fig. 2. Instrument for the measurement of the AC electric field strength at a grounded surface. (1 = capacitive electrode, 2 = insulation, 3 = grounded electrode, 4 = coaxial cable, and 5 = shielding instrument box)

thickness and height of a person can thus be calculated (3). Fig. 1 shows the influence of height and thickness on the capacitive current to a man standing in a 50-Hz homogeneous electric field when the man is approximated with a semi-spheroid.

Instrument for measuring electric field strength at a grounded conducting surface

Gauss' law yields the induced charge density σ at a conducting surface due to the external electric field strength E

$$\sigma = E \varepsilon \varepsilon_0, \quad (5)$$

where $\varepsilon = 1$ for a field in air. If the electric field is alternating with a frequency ω , it can be represented by a displacement current flowing into the surface with a current density j , where

$$j = \omega E \varepsilon \varepsilon_0. \quad (6)$$

This gives a method for measuring field strength at conducting surfaces.

A conducting flat probe can be placed on the grounded surface and connected to the earth via an AC ammeter. The field strength can be calculated from the current flowing into the plate if the area of the plate S and the frequency ω of the field are known:

$$\int_S E \cdot dS = I / \omega \varepsilon \varepsilon_0, \quad (7)$$

where $\varepsilon = 1$ for air or if E is homogeneous over S :

$$E = I / \varepsilon \varepsilon_0 \omega S. \quad (8)$$

For accurate measurements the connection to the ammeter should be shielded and the impedance to earth of the connecting cable should be much greater than the inner impedance of the ammeter. The time constant RC of the ammeter resistance R and the sum of cable capacitance and plate capacitance to earth C should be

$$RC \ll 1/\omega. \quad (9)$$

For a sandwich probe with a grounded electrode below the insulated capacitive electrode, the capacitance is:

$$C_p = S/d(\varepsilon_i \varepsilon_0), \quad (10)$$

where S is the area of the capacitive electrode, d is the thickness of the insulation, and ε_i is the relative dielectric constant of the insulator material.

A field strength measuring system was constructed according to this principle. The field strength probe was a round plate of $3 \cdot 10^{-2} \text{ m}^2$. It was connected to a data precision digital voltmeter via a 1-m coaxial cable. A $10^4 \Omega$ resistor was connected in parallel with the voltmeter. The capacitive current was thus measured with the digital voltmeter (fig. 2). The voltmeter was protected with a combined zener diode — gas discharge tube transient protection. The probe was calibrated for 50 Hz in a known electric field between parallel plates. Similar instruments have been used by Schneider et al. (15) and Miller (14).

The use of the capacitive probe is limited to grounded surfaces because the potential of the probe is that of the ground.

If the probe is put up at space point with a nonzero potential, a strong disturbance of the electric field will be introduced at the measuring point, and too high values are measured (14).

Two capacitive probes arranged as a symmetric dipole can be used for measurement of the field strength at a point with a nonzero potential (8, 15). The current flowing between the plates is then proportional to the time derivative of the field strength component in the dipole direction. Consequently this instrument is direction sensitive. The two dipole halves can be arranged as the two halves of a sphere or a spheroid (14). The dipole introduces a disturbance of the field by short-circuiting part of it. This disturbance and the sensitivity can easily be calculated for spheric or spheroidal dipoles, and they can be measured by calibration for other dipole geometries.

contained the electronics. The electronic circuit of the instrument is shown in fig. 3.

The instrument can be placed at the top of a thin insulating rod with a known height. Useful measurements can also be made with the instrument attached to a 0.5-m long insulating handle, which is held by the hand with the arm outstretched.

Test measurements have also been made with the instrument held in the hand below a long single horizontal EHV conductor. The accuracy of such measurements at a height of 1—2 m proved to be better than 5 %.

It is essential that the instrument be corona-free during measurements. In an electric field E_y (kV/m) the approximate voltage disturbance U_d of the space potential at one end of the dipole will be $U_d \approx E_y \cdot d/2$ (kV), where d is the length of the dipole. For $E_y = 50$ kV/m and $d = 0.1$ m, U_d will be 2.5 kV. This voltage does not cause any corona discharges from the rounded corners of the instrument case.

Capacitive currents to a person in the electric field

The capacitive current to a person standing in an alternating electric field can be measured by connecting him to the ground potential via an AC ammeter. He must, however, wear insulating shoes during the measurement. The measured current will be on the order of $14 \mu\text{A/kV/m}$ for a 50-Hz field. It must be remembered, however, that other people standing near this person will disturb the electric field and thus the capacitive current.

Capacitive current measurements on a man of normal height can thus be used for rough but simple measurements of the mean field strength near the ground. A mean field strength value of about $70 \text{ V/m}/\mu\text{A}$ (50 Hz) can be used for the field strength calculation from the capacitive current when a man, 1.8 m tall, is standing upright in the field with his arms down. A dummy has been built for measurements of the internal distribution of the capacitive current to a man. The insulated dummy is painted with a semi-conducting paint with a surface resistivity of about $1,000 \Omega$ per square. Its arms, legs, torso, and the two halves of its head are insulated from each other and connected to a central unit in the torso. At a junction in the central unit different connections of the body parts can be connected to one of three transient protected digital AC ammeters for the measurement of the currents between different parts of the body. The dummy can be connected to the ground via one hand or one foot. The "current distributions" in the body are thus measured for different ground contact points. The digital ammeters are visible

through a shielding metal net at the front of the dummy (fig. 5).

The dummy can be set up in various natural work positions: upright or bent, with the arms down or with one or two arms up. Electrically connecting hand-tools can be attached to one hand. The

Fig. 4. Instrument for measurement of the AC electric field strength at points with nonzero potential — front panel.

Fig. 5. Dummy for measurement of the distribution of capacitive currents to different parts of the body.

Table 1. Electric field strengths, in a 400-kV substation, measured with the capacitive probe at the ground E_0 and on top of the head of a man $E_{1,800}$.

Construction part	Distance (m)	E_0 (kV/m)	$E_{1,800}$ (kV/m)
Disconnecter busbar (new)	3	8.8	77
Disconnecter busbar (old)	2	12	89
Circuit breaker	1	3.5	65
	4	9.4	73
	6	8.3	59
	16	—	22

shielding effect of different dry or wet clothes can be investigated with the dummy, as well as the effectiveness of the special shielding apparel constructed for EHV work.

RESULTS

The capacitive probe was used for several measurements in substations. Table 1 shows the electric fields measured at the ground near different construction parts in a substation. It also shows the electric field strength on top of the head of a person, 1.8 m tall, standing at the same positions.

The probe proved to be very simple to use, but, as the measurements were

limited to grounded surfaces, it was impossible to use under certain conditions, e.g., when the ground was covered with high grass or snow. The electric field strength at the ground is furthermore very inhomogeneous due to the local topography of the ground. The probe is, however, convenient for measurements at constructions or on the surface of various objects like vehicles.

The dipole probe was only used for the mapping of the field strengths in one substation. It is very easy and rapid to use, held by the hand, and the accuracy of this method of operation is satisfactory. Fig. 6 shows a map of the field strengths measured at a height of 1.8 m in a 400 kV substation. The values measured at the Swedish 400 kV substation have been compared to values reported from measurements in the U.S.S.R. (7, 8). The values obtained agree within 30 %. A preliminary measurement has been made of the field strengths in a 220 kV substation. It shows that the field strengths at a height of 1.8 m are approximately half of those in the 400 kV substation. The measurements made in the U.S.S.R. also show a rapid increase in the field strengths at a height of 1.8 m with the operating voltage (7).

Capacitive current distribution

The capacitive current distribution to a person in an electric field was measured with the dummy at two different places in a substation with different field strengths at the ground, 8.6 kV/m and 18 kV/m, respectively. Table 2 shows the currents measured in different parts of the body for two attitudes of the body and for the dummy insulated or connect-

Fig. 6. Electric field strengths in a 400 kV substation. (1 = steel tower, 2 = disconnector busbar, and 3 = circuit breaker)

ed to the ground via one hand or one foot. The total current to the ground was measured. The values are shown in table 3, they are compared to those reported by other authors and to the theoretically calculated value for a person 1.75 m tall.

DISCUSSION

The measurements that will be made during the study of EHV substations will cover substations of different ages and types of construction. A special survey will be necessary for the groups doing maintenance work at circuit breakers. As the work is done partly on top of the breakers, this survey should cover the whole-breaker constructions at different heights.

A study of the time required for different types of work in the work areas in different field strength zones will follow the field strength measurements. The exposure to the field strengths can then be calculated.

Practical measurements of electrical discharges to persons during ordinary work are very inconvenient since the measuring equipment must be connected both to the persons studied and to the earth and this set-up involves certain hazards. Such measurements are planned, however.

The mean intensity of the discharges can be calculated. The number of discharges does certainly vary widely for different types of work and clothing.

It has been recommended in the U.S.S.R. that all discharges to personnel be elim-

Table 2. Capacitive currents to different parts of a dummy.

Position	Ground connection	Current measured	E = 8.6 kV/m I (μ A)	E = 18 kV/m I (μ A)
Arms down	insulated	head to torso	20	—
		arms » »	14	—
		legs » »	58	132
One arm up	insulated	head » »	20	45
		arms » »	30	49
		legs » »	74	158
Arms down	to one arm	head » »	26	51
		arms » »	61	165
		legs » »	11	13
One arm up	to one arm	head » »	24	48
		arms » »	66	140
		legs » »	11	13
Arms down	to one leg	head » »	26	51
		arms » »	23	47
		legs » »	85	186
One arm up	to one leg	head » »	24	50
		arms » »	41	103
		legs » »	89	233

Table 3. Capacitive current to a man exposed to a 50-Hz homogeneous field strength of 1 kV/m.

Measurement	Author	I (μ A)
Measured for a group of men mean height = 1,750 mm	Schneider et al. (15)	14
Measured for a cylinder height = 1,750 mm, diameter = 250 mm	Schneider et al. (15)	14
Measured with the dummy	Lövstrand (present investigation)	12
Measured in a substation	Filippov and Morozov (8)	10
Calculated for a semispheroid height = 1,750 mm, diameter = 400 mm	Lövstrand (present investigation)	14

inated. This seems to be an unrealistic requirement.

At present the exposure to field strengths is recommended for use as the single parameter of stress related to the EHV. The constructed instruments make measurements of this exposure possible. A correlation analysis can thus be made of exposure to field strengths of the personnel and the observed health deviations, if any, by the medical investigation.

If any negative health effects are found in the investigation, it might be necessary to limit occupational exposure to electric fields. It is possible to decrease the field strengths with various types of shields or shielding clothes. The use of such are discussed in reports from the U.S.S.R. (8). The dipole instrument can then be useful as a control instrument for occupational safety since it is reliable and simple to use.

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